

# $D^0$ cross section and $R_{AA}$ in Isobar

2022.3.28

# Bin centering scale factors

Levy func:

$$\frac{A(n-1)(n-2)}{nT(nT + m_0(n-2))} \times \left(1 + \frac{m_T - m_0}{nT}\right)^{-n}$$

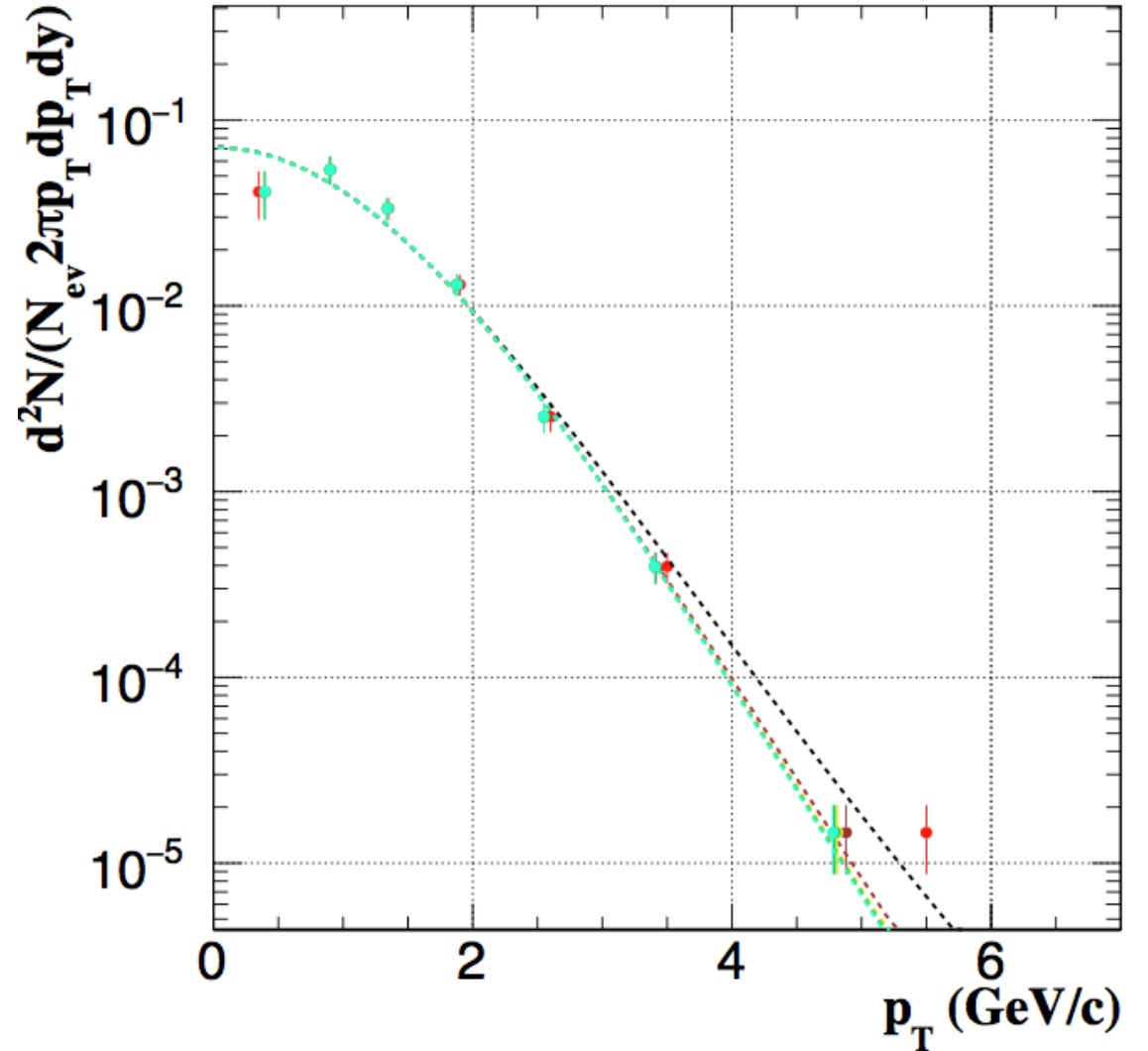
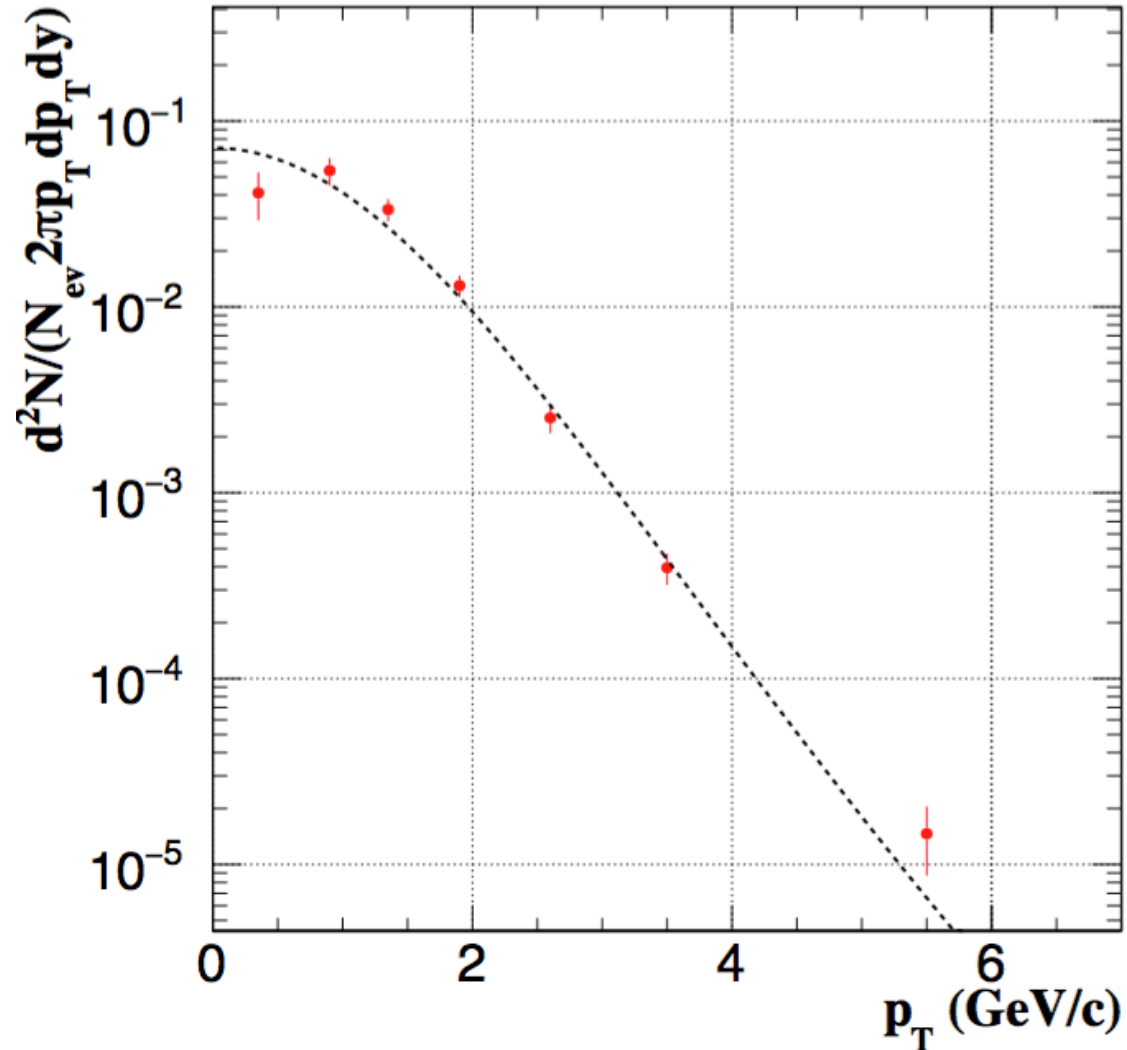
1. The measured yield, initially plotted at the bin centers, is approximated by Levy func;
2. To each bin a momentum  $p_T^*$  was assigned as calculated from the equation;

$$f(p_T^*) = \frac{1}{\Delta p_T} \int_{\Delta p_T} f(x) dx$$

3. Re-fitted  $p_T^*$  as the abscissa. This procedure was re-iterated until the values of  $p_T^*$  were stable.

# Bin centering scale factors (RuRu)

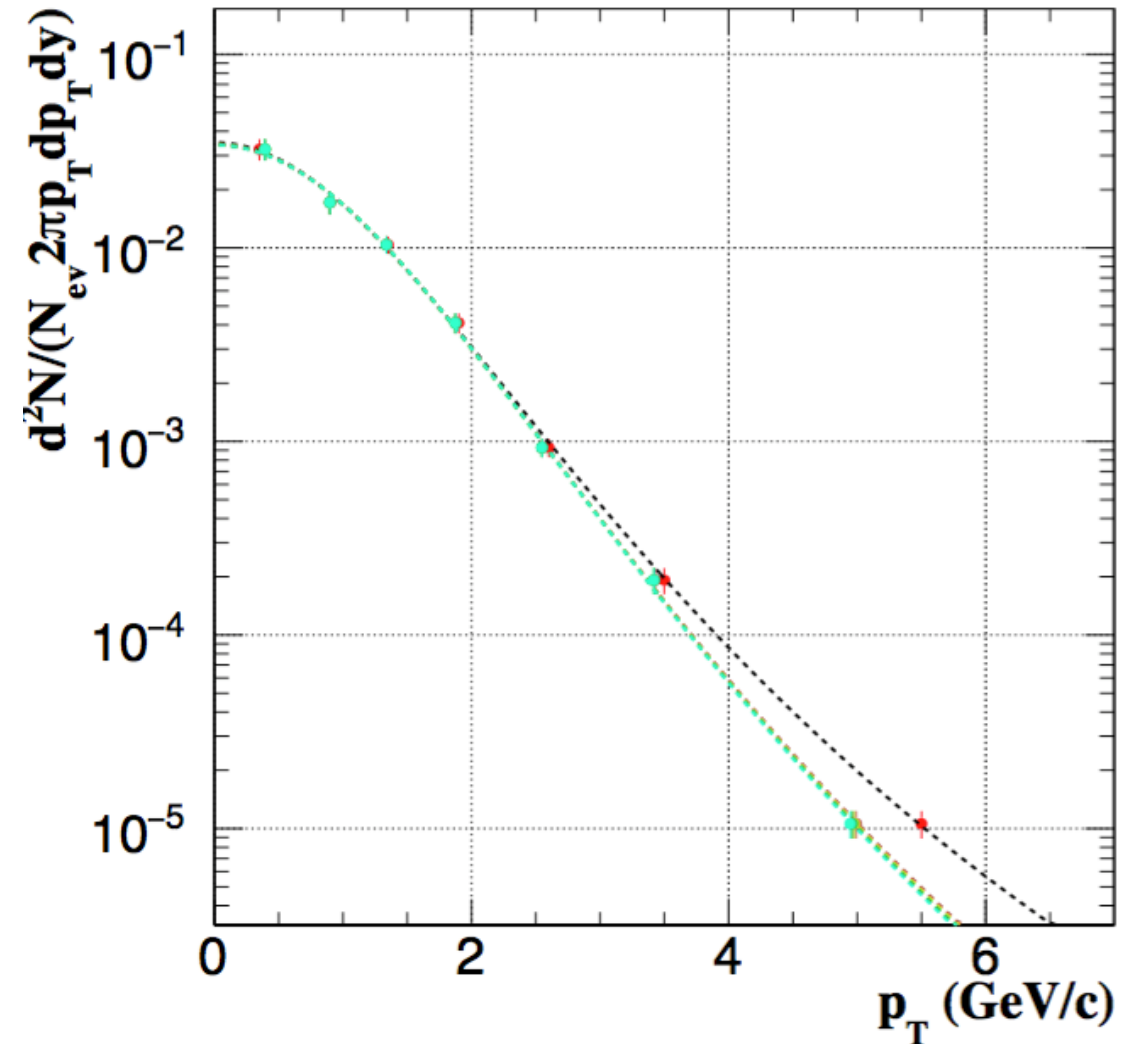
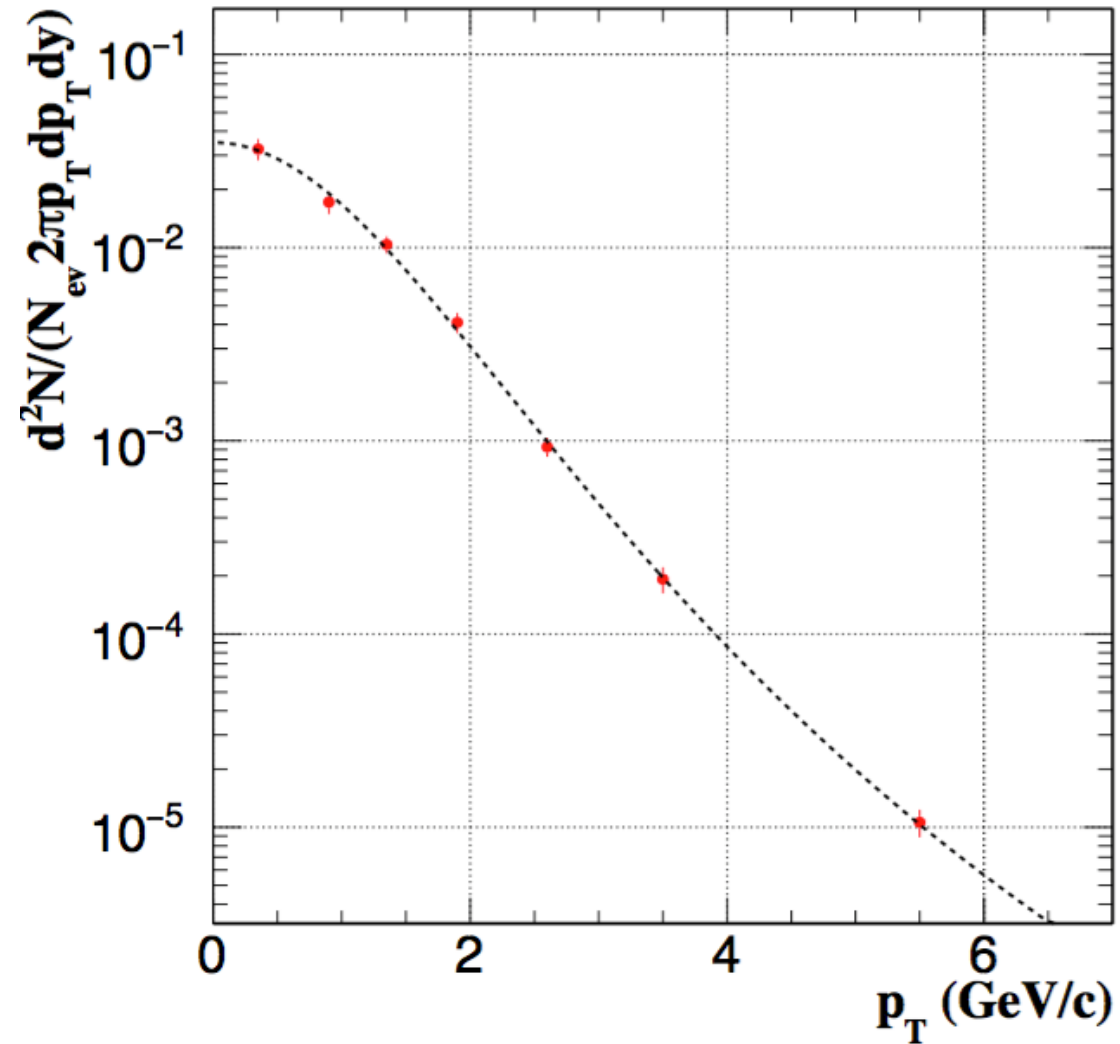
0-10%



Narrow bin width will increase the precision.

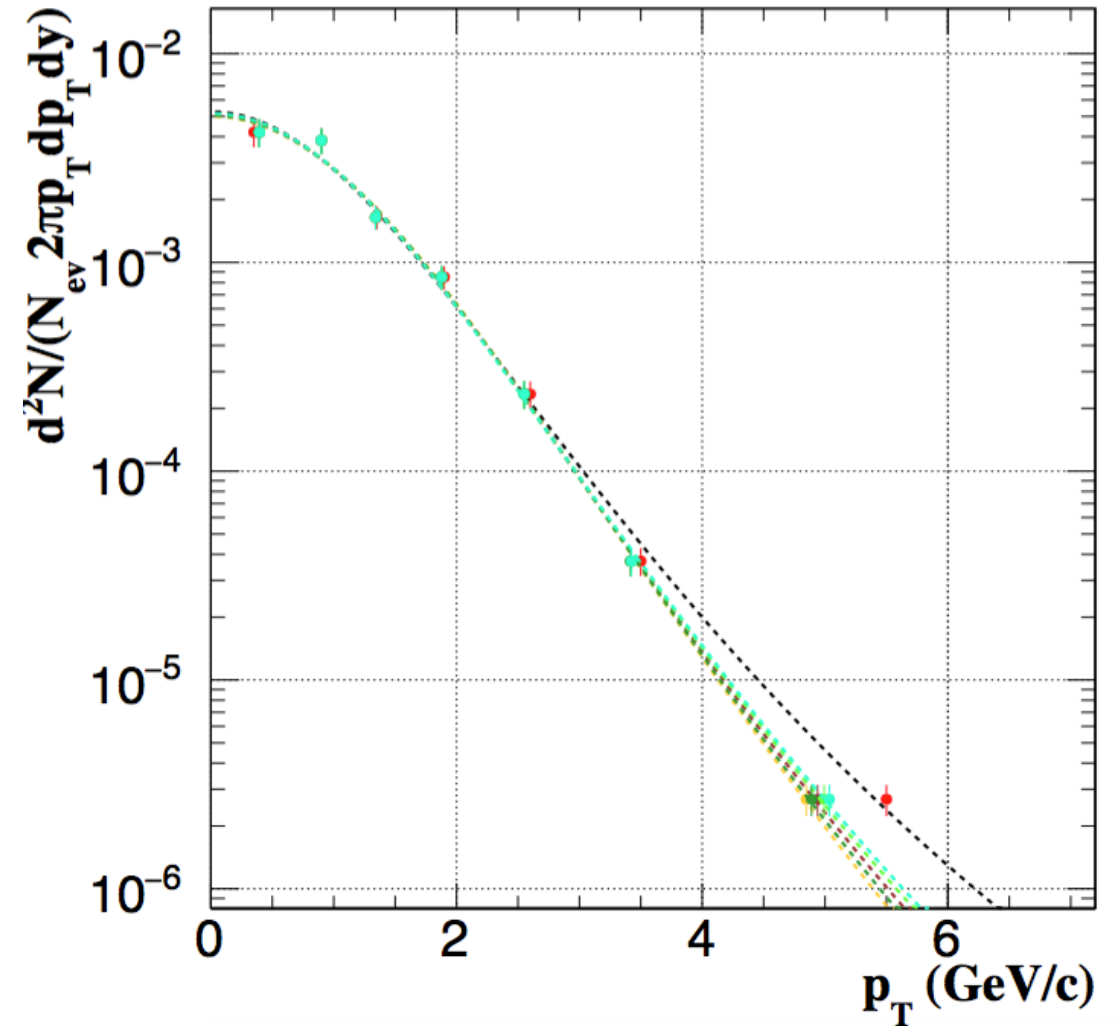
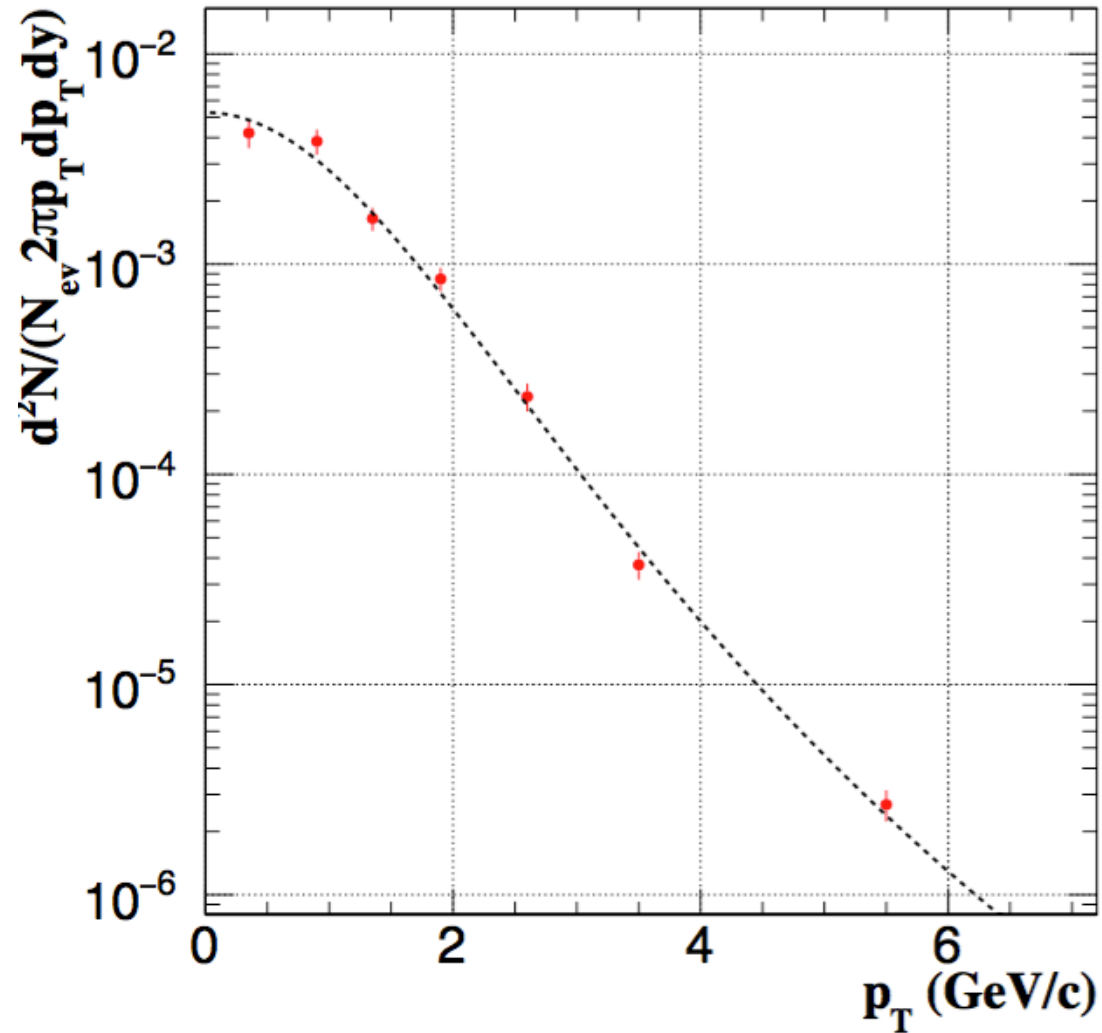
# Bin centering scale factors (RuRu)

10-40%

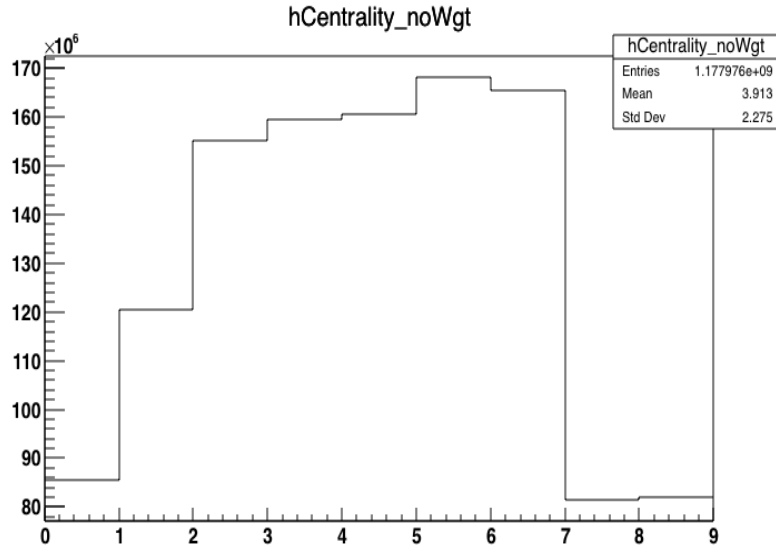


# Bin centering scale factors (RuRu)

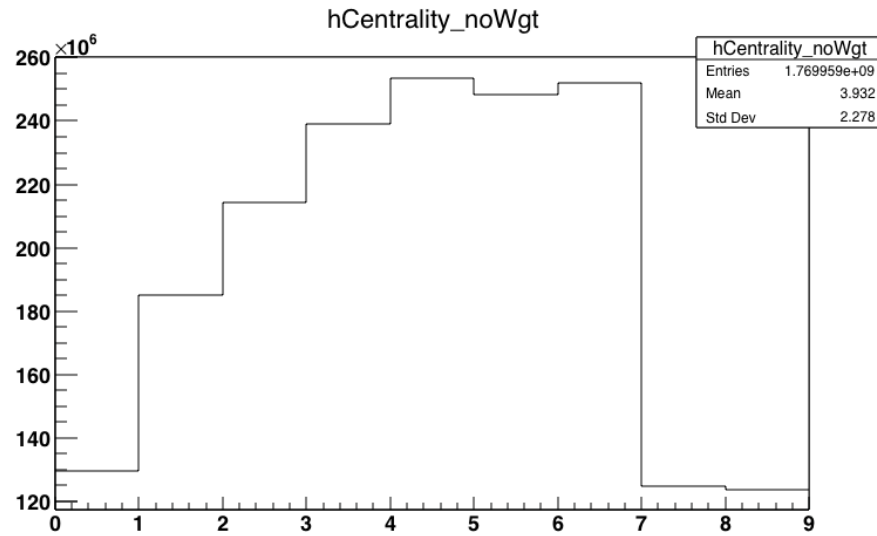
40-80%



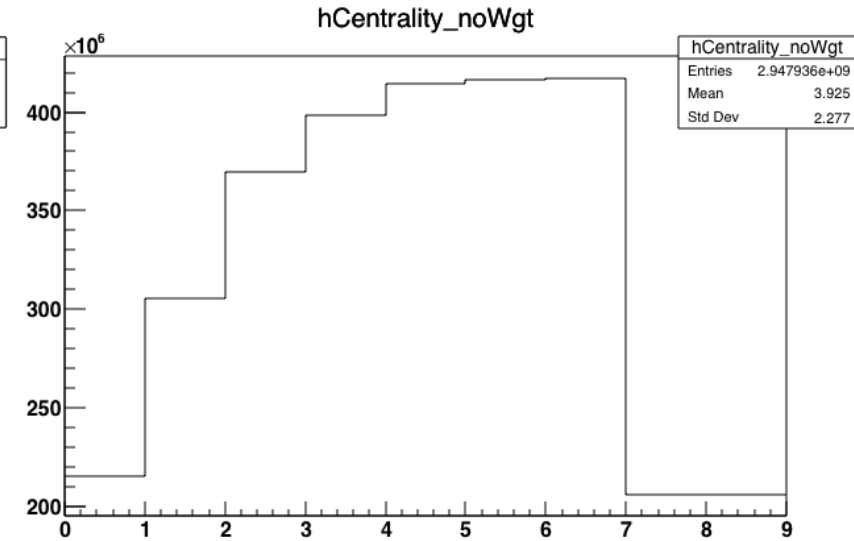
# $D^0$ spectra in ZrZr & RuRu



0.2-7 GeV/c (RuRu)



0.2-8 GeV/c (ZrZr)



0.2-8 GeV/c (Isobar)

# $D^0 R_{AA}$

Motivation:

As a function of  $p_T$ : large  $p_T$   $D^0$  typically originate from hard processes, and then interact with dense and hot medium, lead to **energy loss ( $R_{AA}$  probe)** of the fast moving quark or gluon.

$$R_{AA} = \frac{d^2 N_{AA}^{D^0} / dp_T dy}{\langle T_{AA} \rangle d^2 \sigma^{PP} / dp_T dy} = \frac{\sigma_{inel}^{NN} d^2 N_{AA}^{D^0} / dp_T dy}{\langle N_{coll} \rangle d^2 \sigma^{PP} / dp_T dy}$$

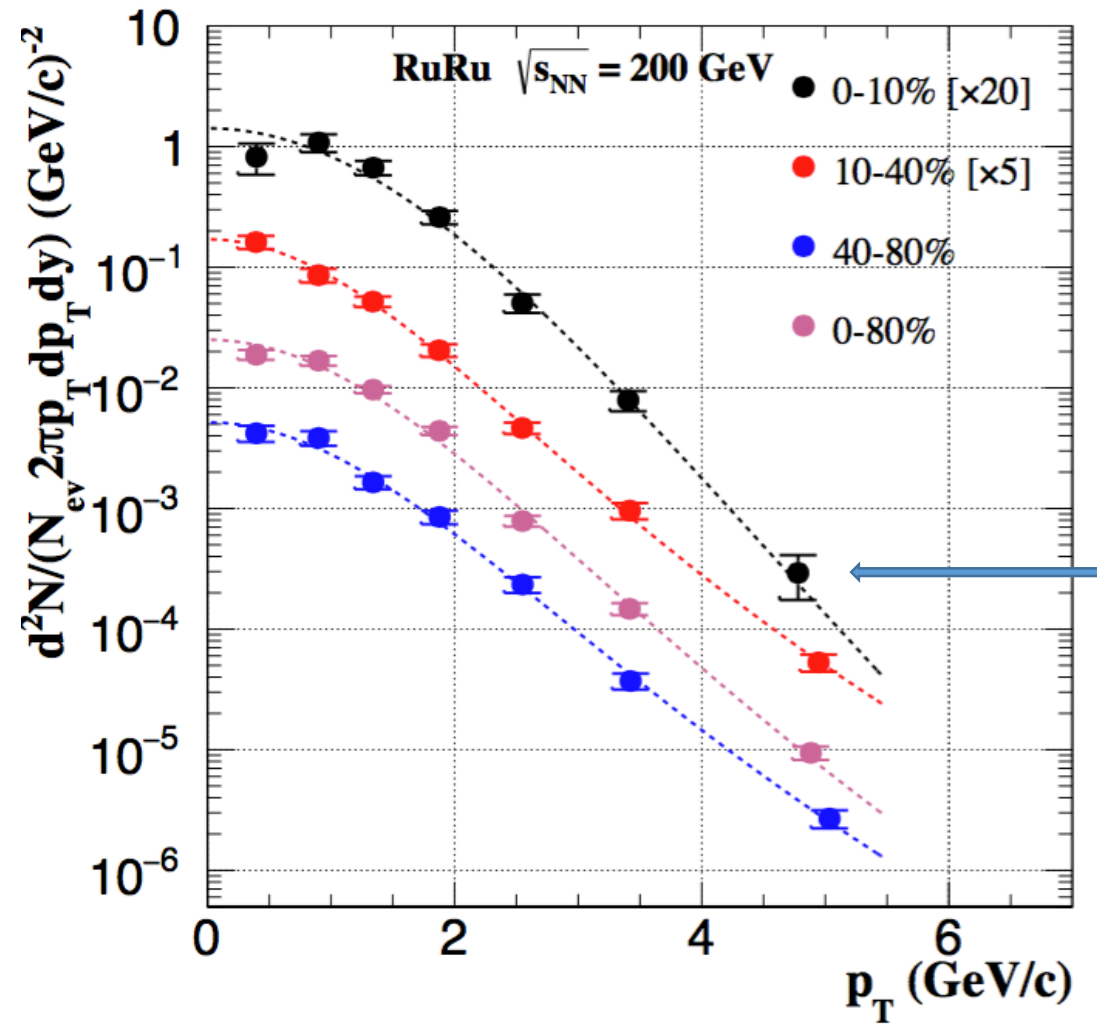
$$\langle T_{AA} \rangle \times \sigma_{inel}^{NN} = \langle N_{coll} \rangle \quad 42 \text{ mb}$$

The yield (or number of particles per event) in Zr-Zr and pp collisions;

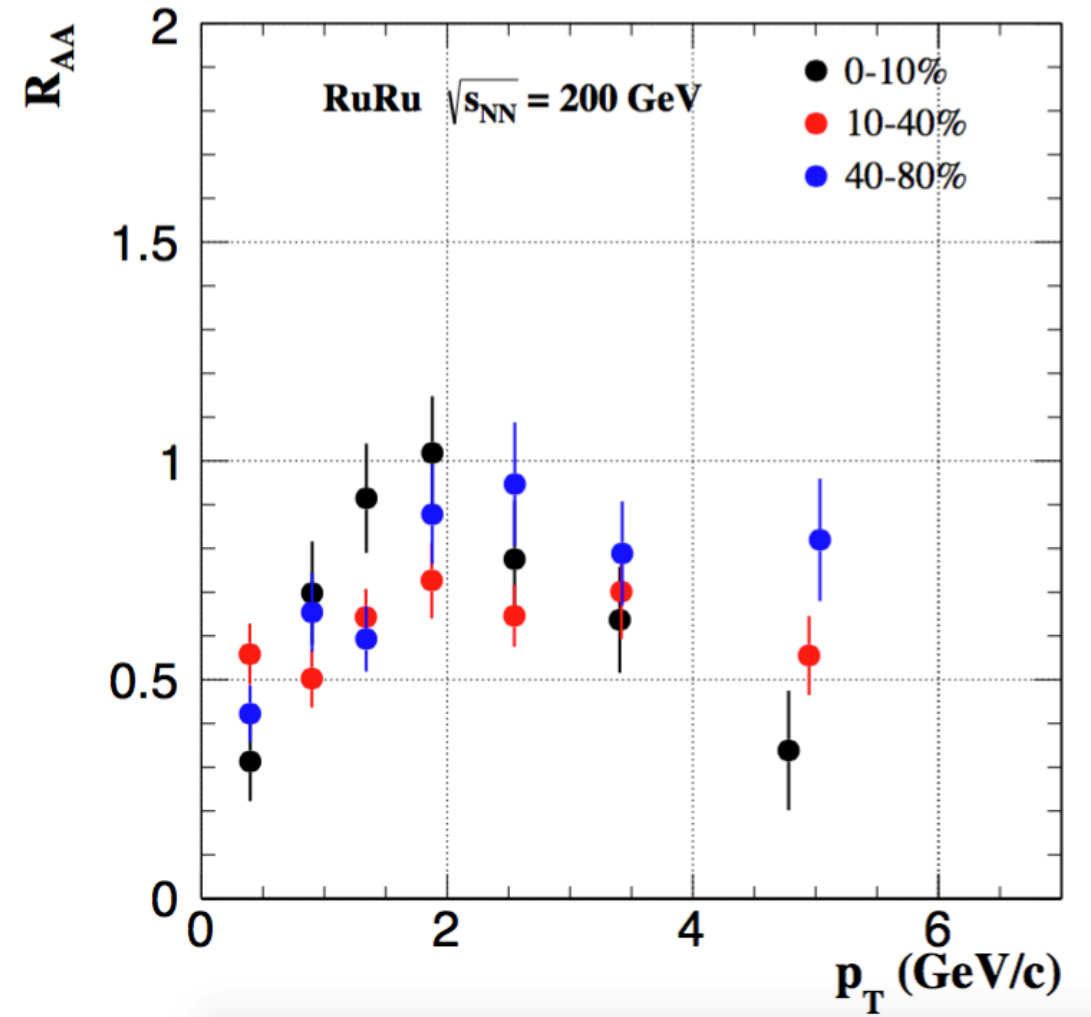
The number of pp collisions should be equivalent on average to one Zr-Zr collision (experiment & Glauber model)

$$R_{AA} = \frac{Y(\text{ZrZr})}{\langle N_{coll} \rangle Y(pp)}$$

# $D^0$ spectra in ZrZr & RuRu

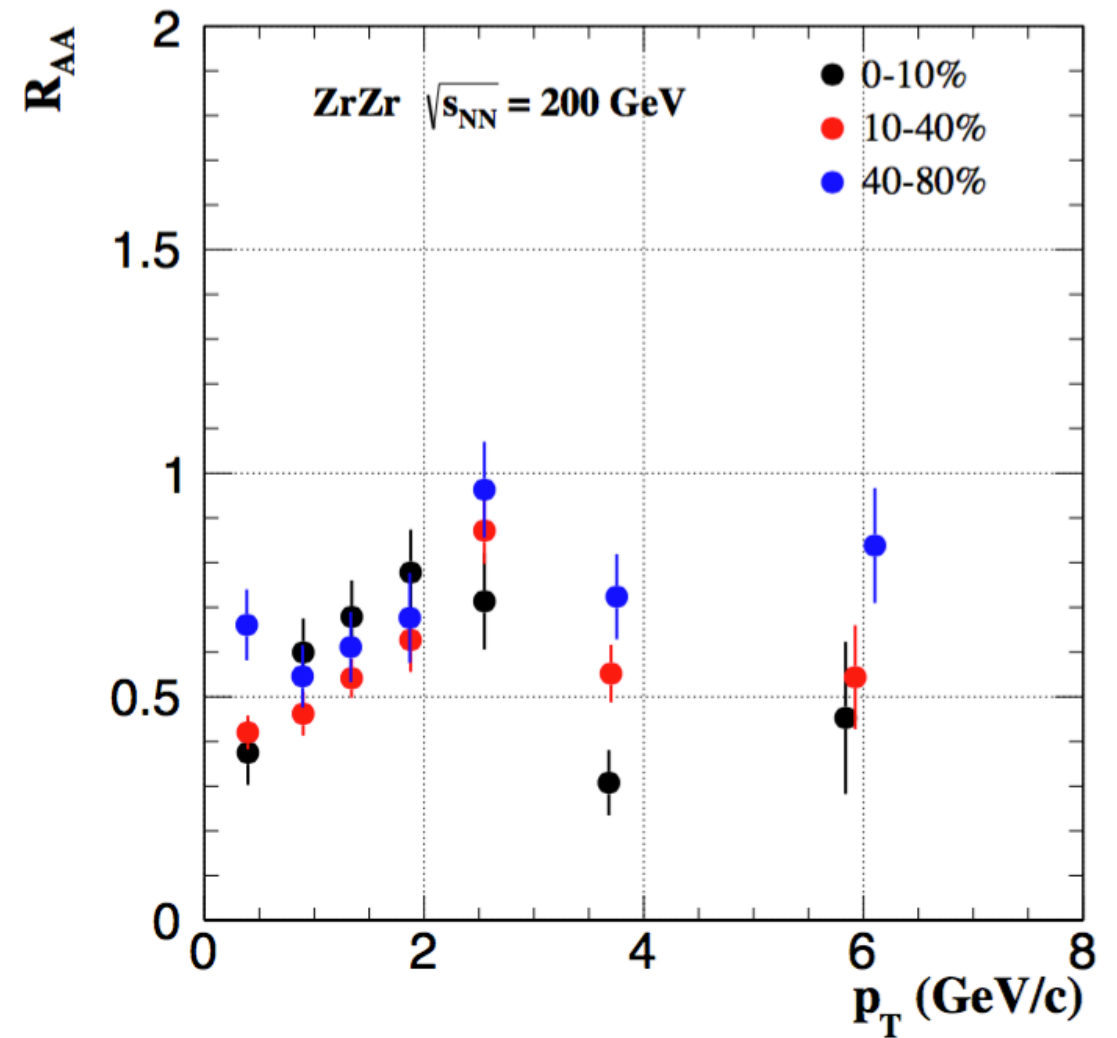
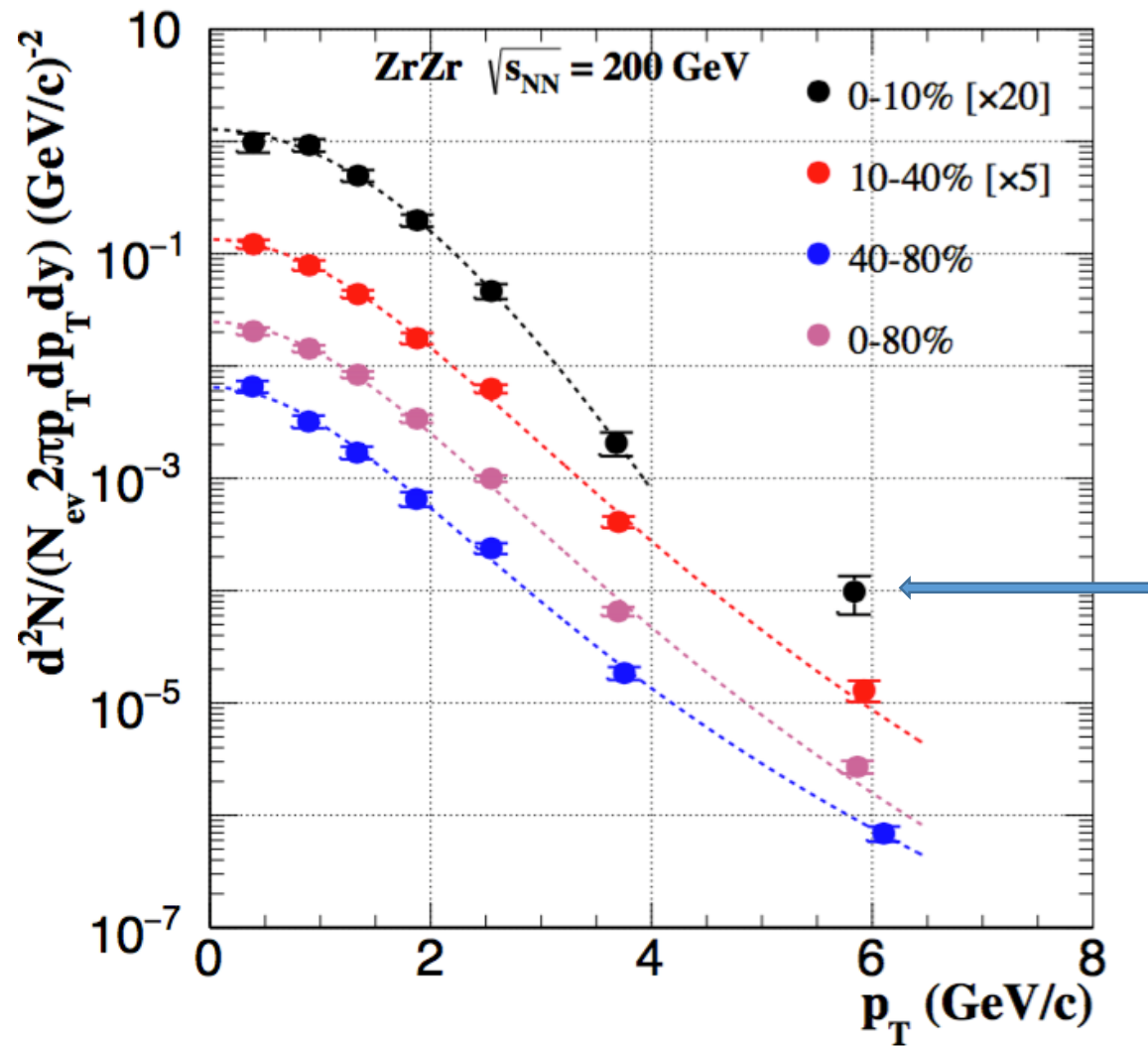


Strict Tofpid cut

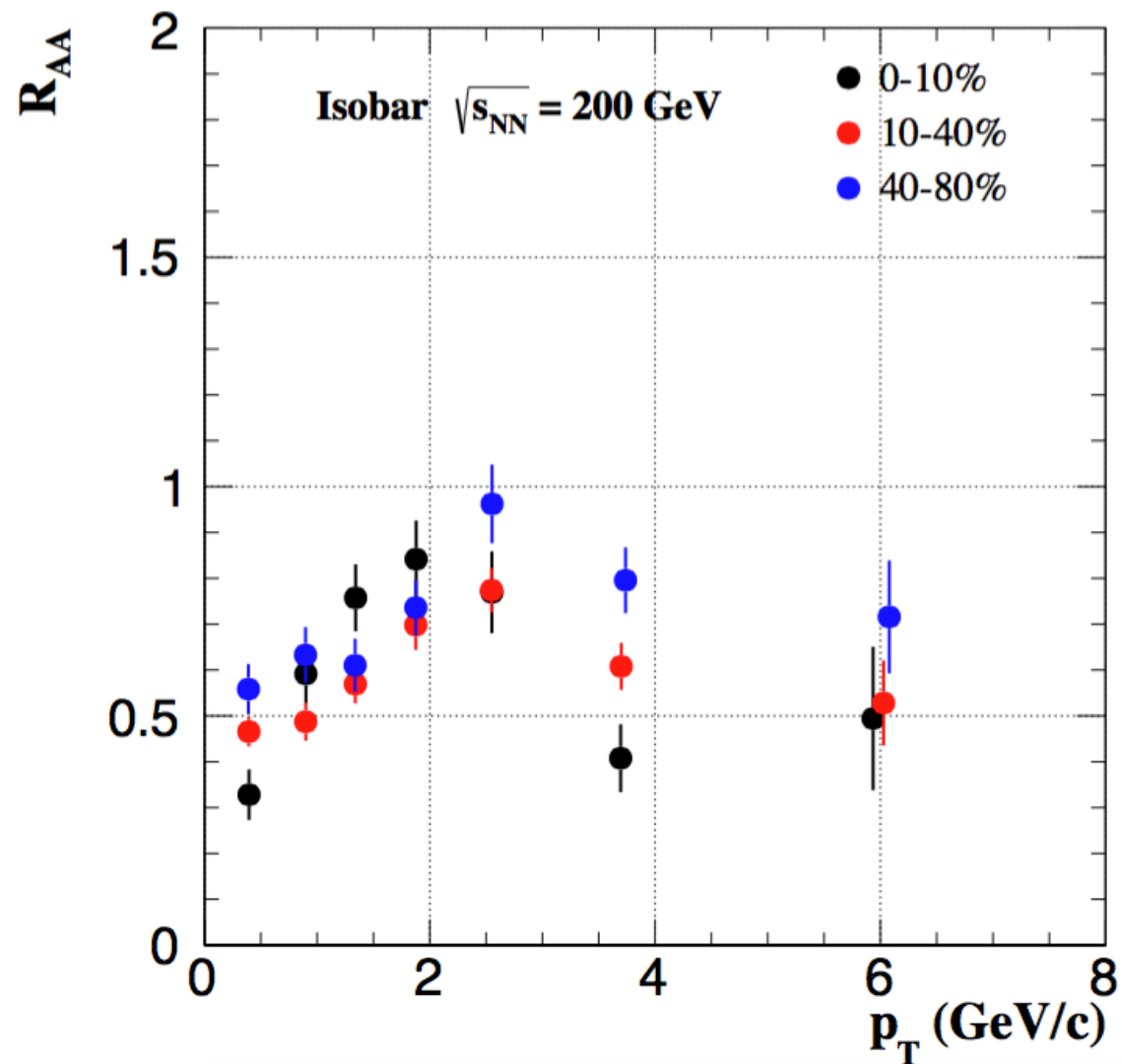
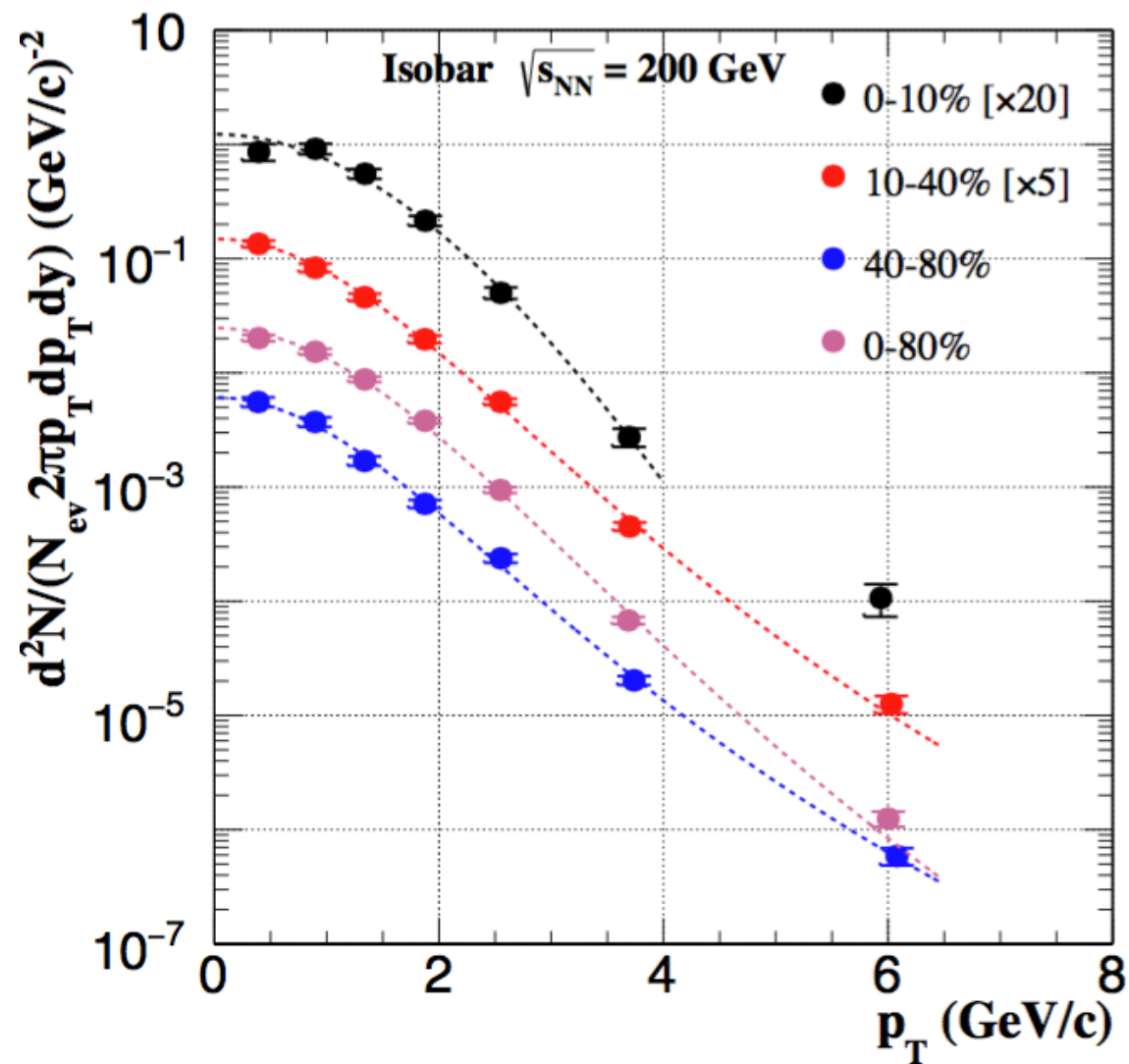




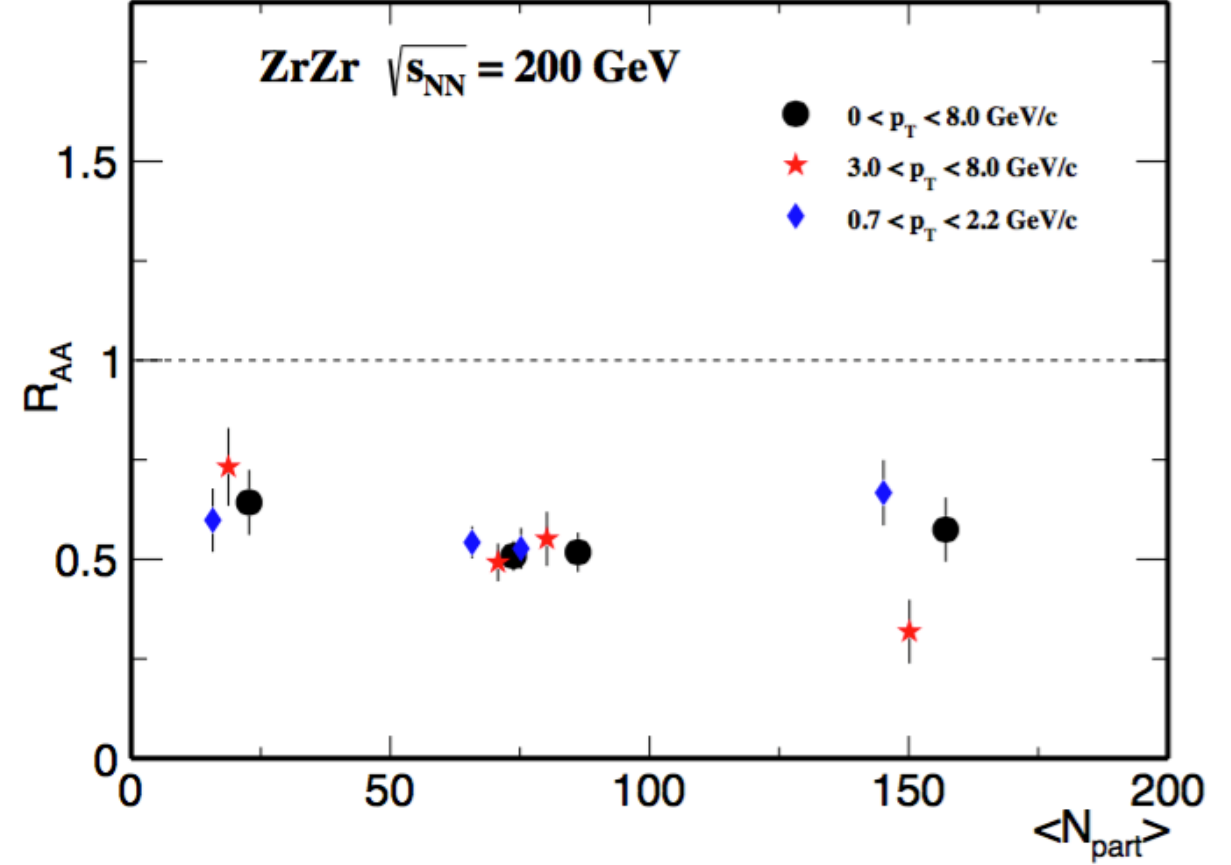
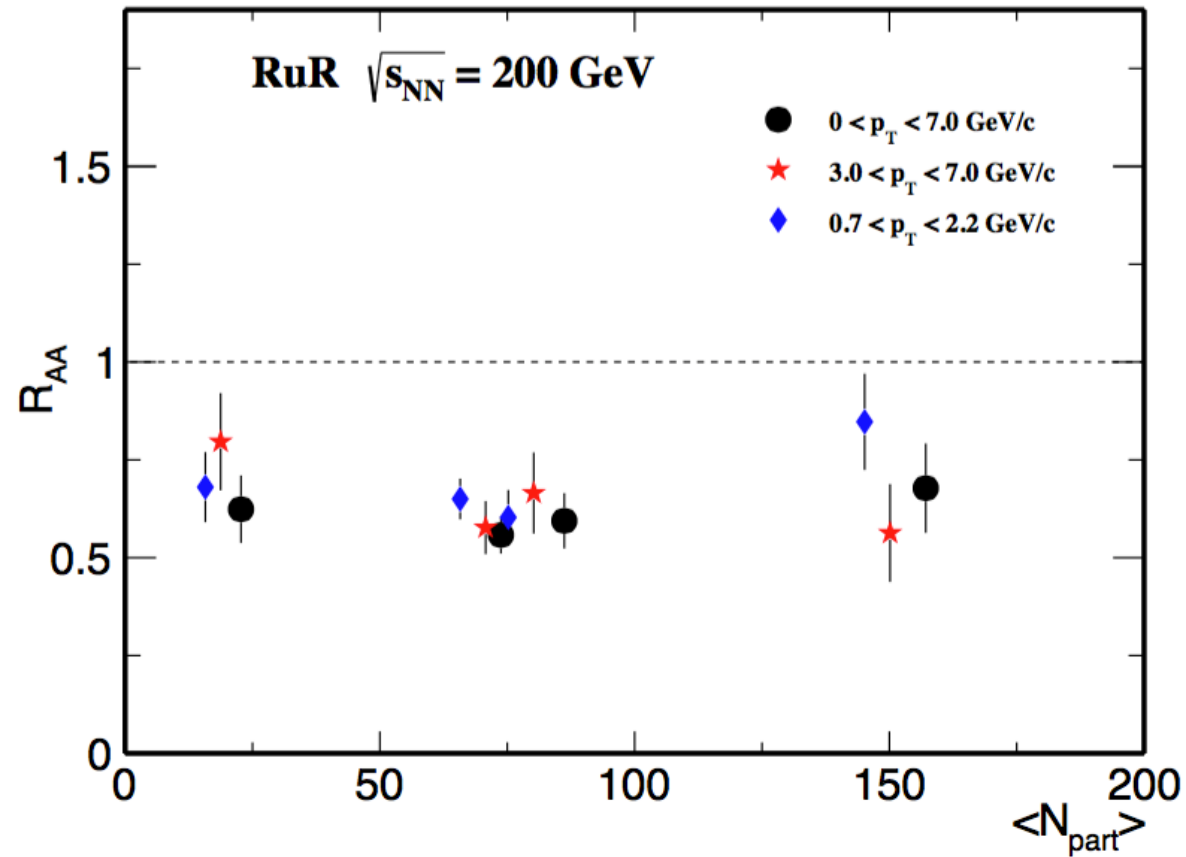
# $D^0$ spectra in ZrZr & RuRu



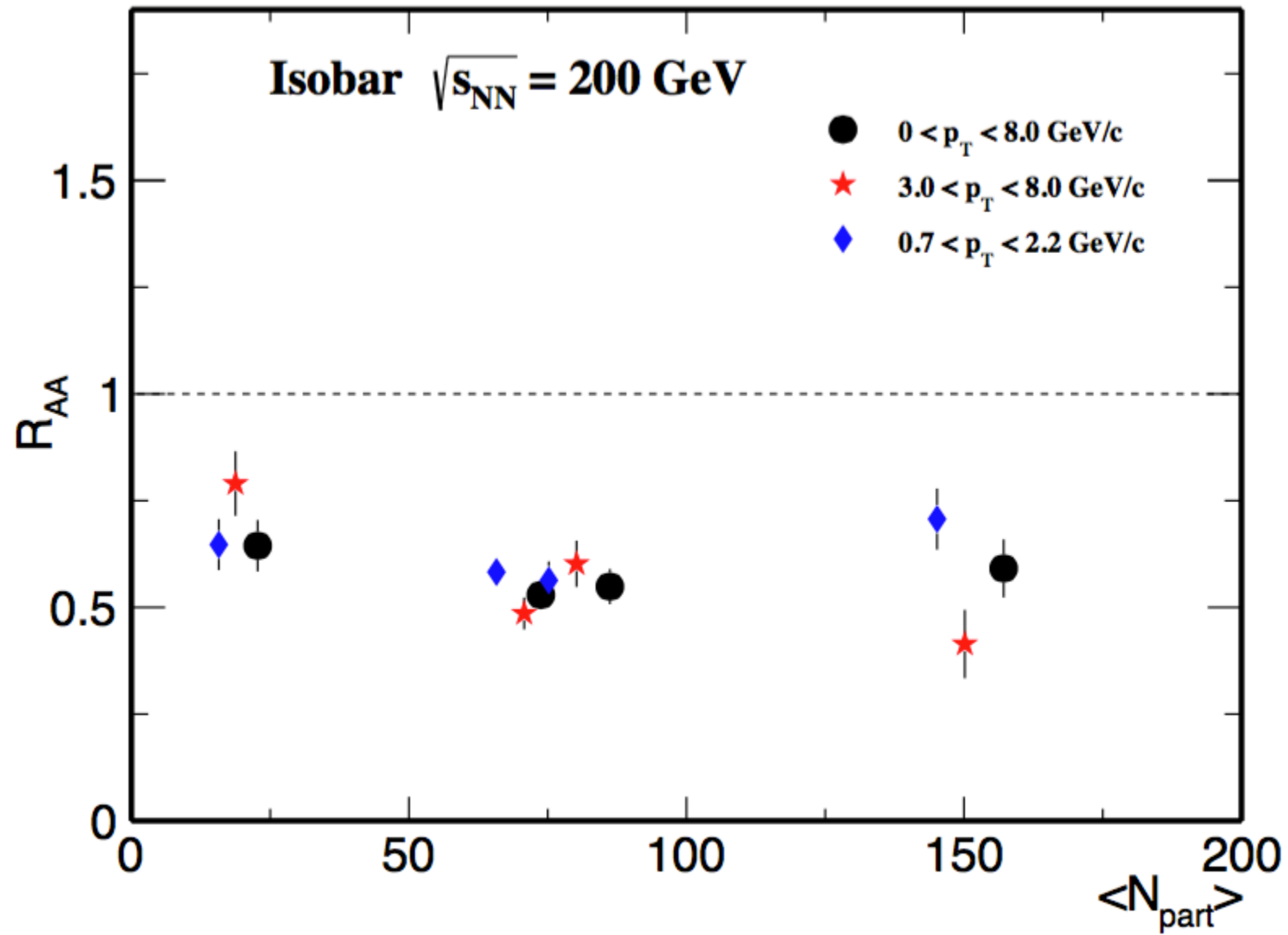
# $D^0$ spectra in Isobar



# $D^0 R_{AA}$ as a function of $\langle N_{part} \rangle$



# $D^0$ $R_{AA}$ as a function of $\langle N_{part} \rangle$



# $D^0$ invariant yield and cross section

The invariant yield of  $D^0$  per one minimum bias collision as a function of the transverse momentum:  
(The Lorentz invariant differential single particle **inclusive cross section**)

$$E \frac{d^3 N}{d\mathbf{p}^3} = \frac{d^3 N}{p_T dp_T dy d\phi} = \frac{d^2 N}{2\pi p_T dp_T dy}$$

$\Phi$  uniform (check for  $D^0$ );  
isotropic production in azimuth  $\sim$  Flow.

$$\frac{d^2 N}{2\pi p_T dp_T dy} = \frac{\Delta N^{raw} / \epsilon_{D^0}^{tot} / 2}{2\pi p_T \Delta p_T \Delta y \times N_{events} \times B.R.} = \frac{\Delta N_{D^0}^{AA}}{2\pi p_T \Delta p_T \Delta y} = E \frac{d^3 \sigma_{D^0}^{AA}}{d\mathbf{p}^3}$$

$$\frac{dN_{D^0}^{AA}}{dy} \Big|_{y=0} = \frac{\Delta N^{raw} / \epsilon_{D^0}^{tot} / 2}{\Delta y \times N_{events} \times B.R.} \quad \frac{d\sigma_{D^0}^{NN}}{dy} \Big|_{y=0} = \frac{dN_{D^0}^{AA}}{dy} \Big|_{y=0} \times \frac{\sigma_{inel}^{pp}}{\langle N_{bin} \rangle}$$

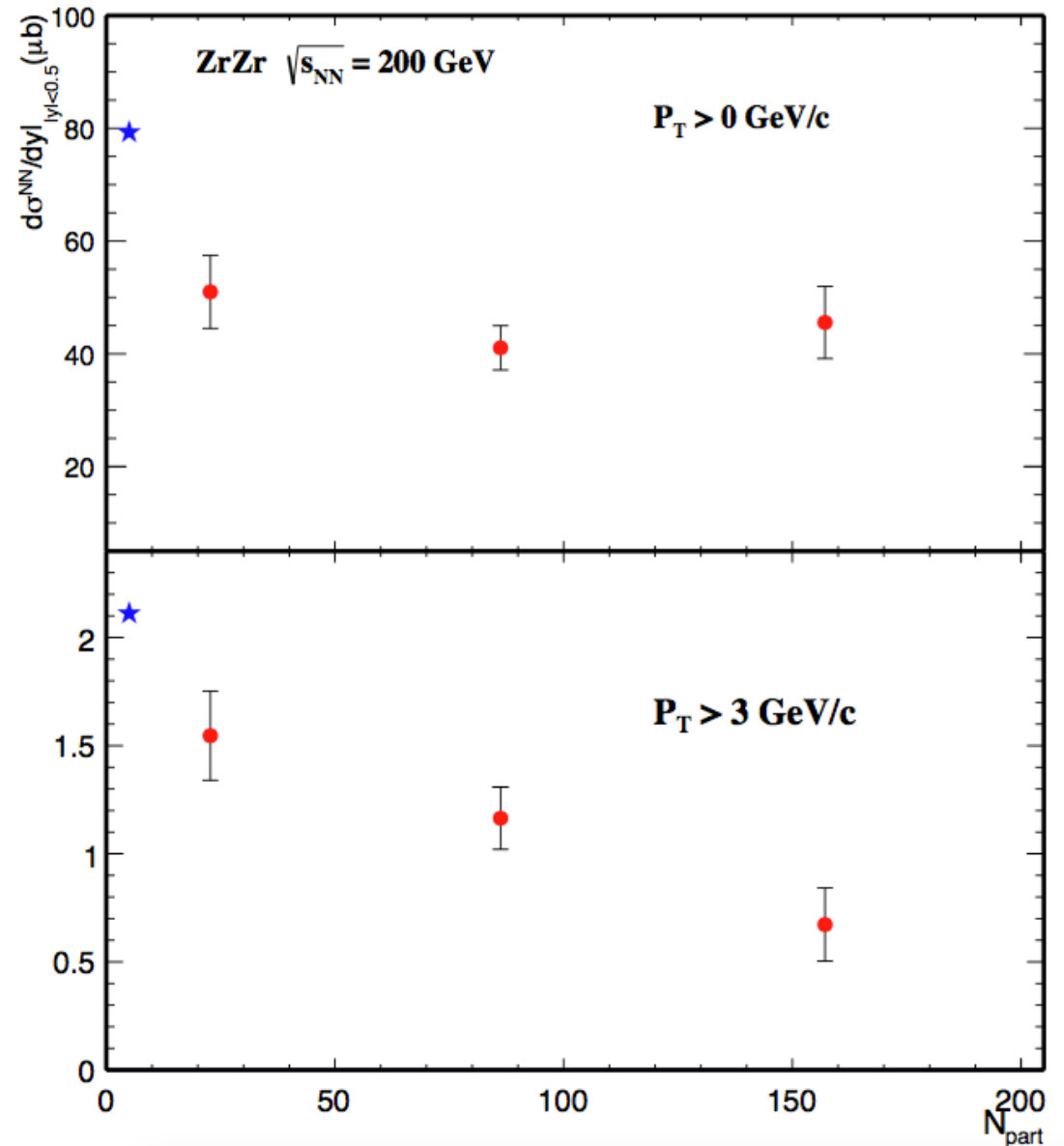
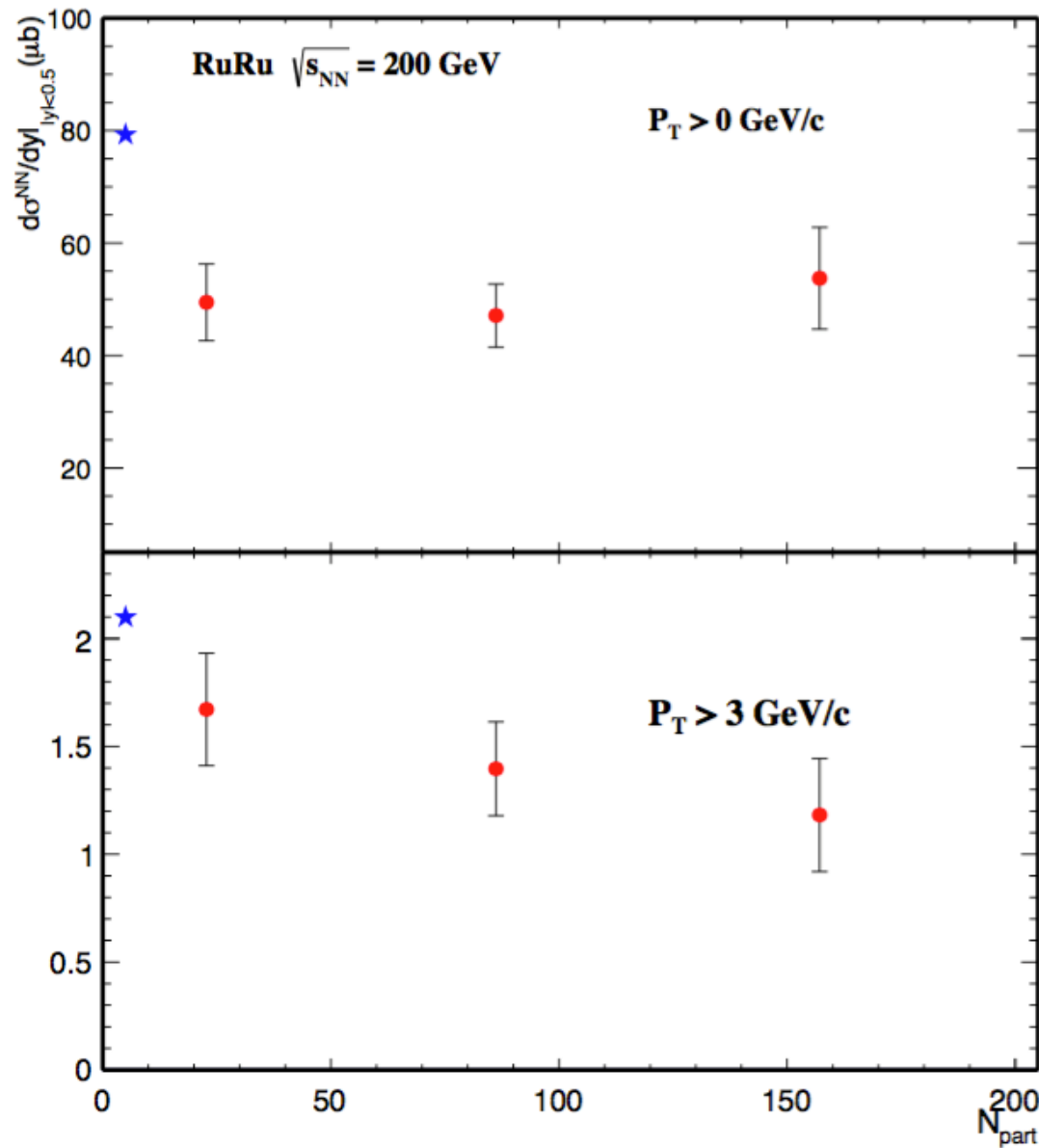
$\Delta N^{raw}$  is the raw yield measured in the bin  $\Delta p_T \Delta y$  ;

$\Delta p_T$  is the  $p_T$  bin for which the yield is calculated;

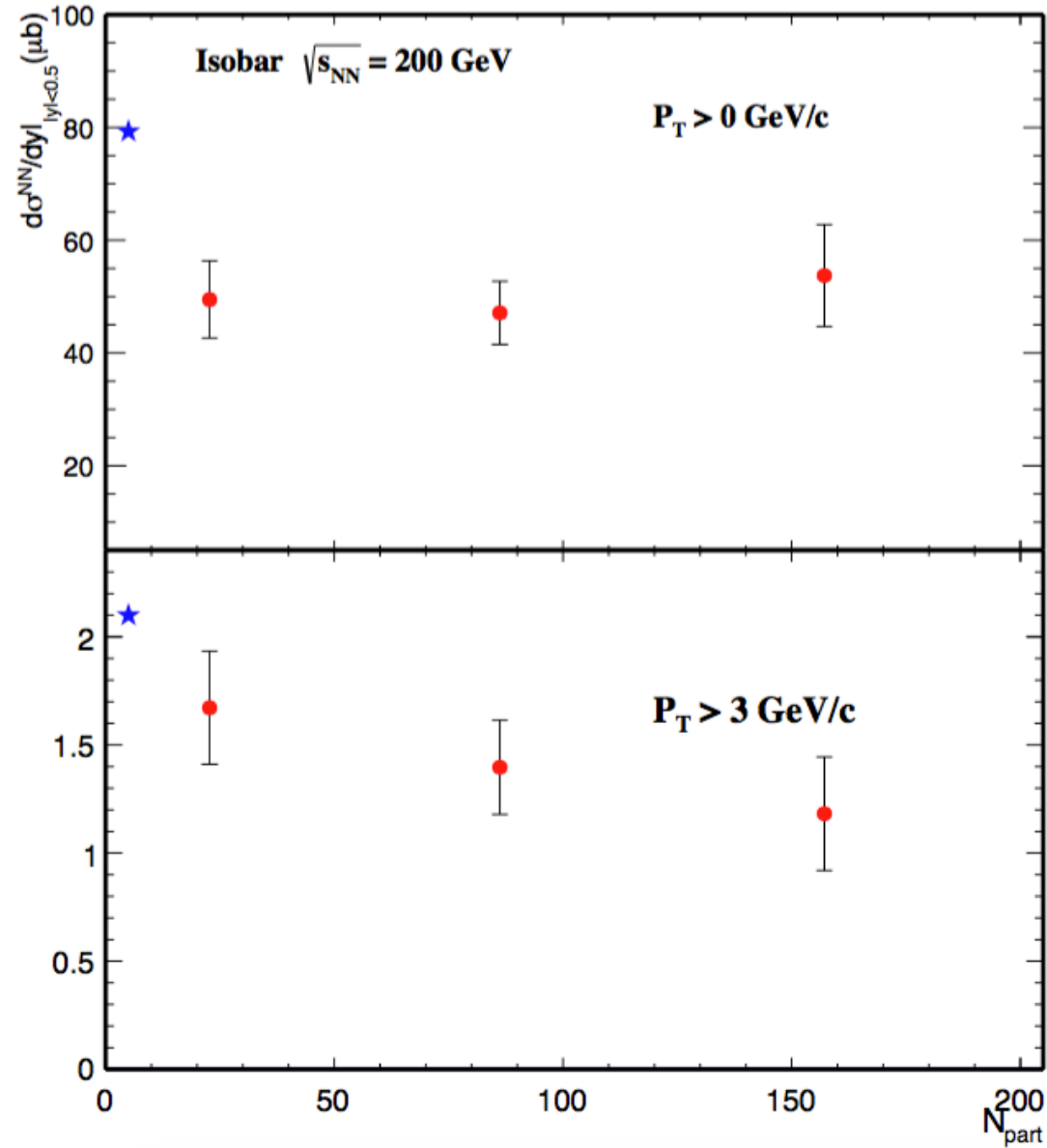
$\Delta y$  is the rapidity range of the measurements, in this analysis  $\Delta y = 2$ ; (check)

$B.R.$  is the branching ratio of the  $K^- \pi^+$  decay channel.

# $D^0$ cross section as a function of $N_{part}$



# $D^0$ cross section as a function of $N_{part}$



Some issues should be considered for  $p_T < 0.2$  GeV/c.

# Strict checks

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- Primary vtx efficiency;
- Double counting analysis;
- $N_{coll}$  and  $N_{part}$  in a wide centrality bin;
- Mean and sigma setting for extracting raw yields;
- Loose cut and sys. Uncertainty.